APPENDIX 6

WATER MANAGEMENT PLAN

Lot 1503 Harris Road, Myalup

Shire of Harvey

Prepared For: Gotam Pty Ltd

Prepared By: Jack Ghasseb

Date: June 2026

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1.0 INTRODUCTION

This Water Management Plan (WMP) supports an Extractive Industries License (EIL) application by Gabi Ghasseb, owner of Lot 1503 Harris Road, Myalup, for the extraction of sand and limestone. It is to be read together with the accompanying report, *Extractive Industries License Application and Environmental Management Plan, Lot 1503 Harris Road, Myalup.

An EIL was previously granted over the property to Omaha Nominees Pty Ltd; that license has since lapsed, and this application re-establishes the operation under the owner's name (Lundstrom Environmental Consultants, 2015). Some sand was extracted under the earlier license before works stopped, but the bulk of the footprint is undisturbed and the water-management setting is essentially unchanged.

The plan sets out the property and its surrounds and their contours and monitoring bores; the extraction programme; the surface-water, storm water and erosion controls; the groundwater regime; the intended post-extraction land use; the potential for effects on Lake Preston; and the potential for acid sulphate soil impacts.

2.0 PROPERTY OWNERSHIP & LOCATION

Property Description: Lot 1503 on Deposited Plan 112302, Harris Road, Myalup, Shire of Harvey

Volume: 1976

Folio: 499

Area: 40.521 ha

Ownership: Gabi Ghasseb *(Written consent for extraction on land Appendix 2)*

The property is situated next to Lake Preston, approximately 2.5 km west of Forrest Highway, and 9 km north of Myalup Township.

3.0 BACKGROUND

The subject land occupies part of the Swan Coastal Plain at Myalup and sits directly to the east of Lake Preston. The characteristics of the property and the land around it are described below.

3.1 CURRENT LAND USE

The lot is held predominantly as pasture. A remnant stand of native vegetation, in the order of 13 hectares, occupies the western part of the property and falls within the Environmentally Sensitive Area associated with Lake Preston. The eastern part of the lot, where extraction is proposed, no longer carries the scattered paddock trees that were once present; these have been removed, and a small quantity of sand was extracted before the operation was suspended. Beyond this limited disturbance the extraction area is unworked and is reverting to pasture grasses. Surrounding landholdings are zoned rural (WAPC, 2019) and are used chiefly for limestone quarrying and general farming. An aerial image of the property and its surrounds appears at Figure 2.

3.2 TOPOGRAPHY & DRAINAGE

The property falls within the Coastal Catchment of the Harvey River Basin (Local Biodiversity Program (LBP), 2025) and is not situated in any Public Drinking Water Source Area. While it lies within a Rights in Water Irrigation Act (RIWI) Groundwater Proclamation Area — specifically the South West Coastal Groundwater Area, Lake Preston North Groundwater Subarea — it sits outside any RIWI Surface Water Proclamation Area (Landgate, 2026).

Lake Preston abuts the eastern boundary of the lot and carries a number of significant designations: it lies within Yalgorup National Park and is recognized as a Lake Conservation wetland, a Ramsar wetland and an Environment Protection Policy (EPP) Lake, and forms part of the lands and waters managed by the Department of Parks and Wildlife.

Several Multiple Use and Resource Enhancement wetlands occur on or near the property (Figure 2). Two small Dampland Multiple Use wetlands sit on the lot itself — one taking in a modest portion of the northwest corner and the other a larger area of the northeast corner. Additional Multiple Use wetlands lie in the surrounding district, including one that contains a Sumpland Resource Enhancement wetland approximately 430 m from the eastern boundary (Landgate, 2026).

Surface drainage over the undisturbed land moves from east to west toward Lake Preston. Ground levels across the property range between 1 and 15 m AHD, and there are no defined surface drainage lines; runoff instead drains internally and infiltrates to the underlying groundwater.

Management of runoff within the project area is dealt with in Section 5.1.

3.3 GEOLOGY AND SOILS

The site falls within the Yoongarillup landform. Shallow, sandy topsoil overlies interbedded limestone, calcarenite, marl and shell beds belonging to the Tamala Formation (WAPC, 2019). Earlier investigations by Commander (1988) indicate the limestone is in the order of 20 to 25 meters thick and rests unconformably on the sands, shales and siltstones of the underlying Leederville Formation. Extraction will be confined to the material lying above the water table.

3.4 GROUNDWATER HYDROLOGY

3.4.1 Data & Information

The nearest formal records are Department of Water and Environmental Regulation (DWER) bores D1 and D2, about 1650 m south and 1640 m southeast of the extraction area (Figure 1). Both begin in 1979; D1 ceased in 2001, while D2 (site 61319145) continues through to 2025. Since 2020 these have been supplemented by a newer monitoring point, LPNSWIM 04-20 (site 61370121). The recorded ranges are summarized in Table 1, with hydrographs reproduced in Addendum 1; all data was drawn from DWER's Water Information Reporting (WIR) system.

Table 1: Summary of Groundwater levels

Bore	Season	~Range (m AHD)	Period
D1 (61319144)	Winter High	-0.22 to 0.19	1994 to 2001
	Summer Low	-0.53 to -0.78	
D2 (61319145)	Winter High	-0.41 to 0.88	1994 to 2014
	Summer Low	0.08 to -0.92	
D2 (61319145)	Winter High	0.91 to ~1.12	2015 to 2025
	Summer Low	-0.53 to -0.65	
LPNSWIM 4-20 (61370121)	Winter High	1.04 to 1.43	2015 to 2025
	Summer Low	-0.32 to -0.43	

To improve the resolution of local data, licensed surveyors established a bench mark beside the soak in the north of the lot (Figure 2). the soak was measured at −0.44 m AHD (23 January 2015), with lake-edge levels of −1.09 m the same day and −0.66 m; from the 0.43 m fall in lake level between those dates, the soak on 2 December 2014 back-calculates to about −0.01 m AHD.

Monitoring at the soak will be ongoing so that the dataset for the site continues to build. The soak will be continuously monitored, allowing for real-time local results. These readings will be in hand well

before extraction advances anywhere near the groundwater level, allowing the design levels to be confirmed against current on-site real time data.

3.4.2 Discussion

The more recent records register higher winter maxima — D2 (61319145) reaching 0.91 to 1.12 m AHD over 2015–2025, and the LPNSWIM 04-20 bore (61370121) 1.04 to 1.43 m AHD over the same period. The adopted level will be constantly monitored by direct on-site monitoring at the soak over the coming winter and the following summer to provide real time data, Because extraction will not advance anywhere near the groundwater level for some time, these real-time local readings will be in hand well before that depth is approached, and the mining and final rehabilitation levels will be set — and adjusted if required — against the confirmed on-site data.

The records show a marked step-down in groundwater levels around 1994, sustained since and generally attributed to a drying climate together with rising irrigation abstraction , with levels from 2015-2025 a slight increase.(Addendum 1). , which best reflects current conditions. Bore D1 — the closest historical analogue to the extraction area, at a comparable distance from the Lake Preston discharge point — recorded a post-1994 winter maximum of 0.191 m AHD (3 November 1994), D2 & LPNSWIM are also close, however have different elevations & topography, however due to the D1 bore being discontinued & accounting for the other bores as well as the local bore, the 0.191m value will be double to 0.382m and this figure is adopted as the maximum groundwater level across the extraction area for the purposes of this proposal.

3.5 RAINFALL

The nearest rainfall station, Lake Preston Lodge 2 Comp. (9679), closed in January 2012 but provides 51 years of record. Mean annual rainfall is 864.4 mm (Table 2), wettest in May–July and driest in December–February; the highest annual total was 1,247.6 mm (1964) and the lowest 486.4 mm (2006). The closest station with more recent data Australind station (9273) was recording 2010-2023 and had a mean of 684.2 mm from 2010-2023. (BoM, 2026).

Table 2: Mean Rainfall Data 9679 & 9273

Station & Period	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	**Annual**
Lake Preston Lodge (1960-2011)	15.8	11.8	18.2	51.6	119.2	172.5	167.0	118.9	82.2	49.3	33.2	13.6	864.4
Australind (2010 - 2023)	19.0	14.9	29.7	50.4	102.5	112.6	130.6	117.9	79.4	37.8	30.2	20.6	684.2

For storm water design, the 2-hour, 10-year ARI intensity for the property is taken as 17.5 mm/hr from the BoM Intensity-Frequency-Duration system (BoM, 2026). DWER guidance requires runoff from this event, generated within the mined area, to be retained within the pit (DoW, 2018) (See 5.2).

4.0 THE OPERATION AND FINAL LANDFORM

Sand and limestone will be extracted across a footprint of the site is returned to pasture, with rehabilitation carried out progressively as areas of extraction are completed. Topsoil and overburden are retained on site for the purpose; slopes behind the working face are battered to no steeper than 1:6 (vertical to horizontal), taking care not to disturb fringing vegetation; and rehabilitation is undertaken in, or just before, the wet winter.

The mining and final levels are set from the adopted maximum groundwater level of 0.382 m AHD (Section 3.4.2). Excavation stops at 0.491 m AHD — 300 mm above that level, the minimum separation between pit base and maximum seasonal groundwater recommended by DWER (DoW, 2014a) — and the rehabilitated floor is left at 0.691 m AHD, about 0.5 m above the maximum winter water table, meeting the recommended clearance for a future pasture land use (DoW, 2014a).

As set out in Section 3.4.2, this adopted maximum will be confirmed by direct on-site monitoring at the soak over the coming winter and the following summer — well before extraction advances anywhere near the groundwater level. Should that monitoring indicate a higher local maximum, the excavation and final rehabilitation levels will be raised accordingly to preserve the 300 mm and 500 mm separations. This approach were levels are checked against current on-site conditions before that depth is worked is protective of the groundwater resource and the adjoining Lake Preston: rather than locking in a floor now on the older bore data alone, If the soak readings show groundwater is higher than the adopted figure, excavation simply stops higher to keep the 300 mm separation. The final landform is shown at Figure 4.

The only water requirement is for dust suppression, drawn from the soak on the property (Figure 2) under a 5C groundwater abstraction license from DWER. There are no licensed production bores within 100 m of the workings.

4.1 REHABILITATION & FINAL LEVELS

The site is returned to pasture, with rehabilitation carried out progressively as areas of extraction are completed. Topsoil and overburden are retained on site for the purpose; slopes behind the working face are battered to no steeper than 1:6 (vertical to horizontal), taking care not to disturb fringing vegetation; and rehabilitation is undertaken in, or just before, the wet winter.

The mining and final levels are set from the adopted maximum groundwater level of 0.382 m AHD (Section 3.4.2). Rather than working to the bare minimum separations recommended by DWER — 300 mm between the pit base and the maximum seasonal groundwater level, and 500 mm between the final surface and that level — Excavation stops at 1.4 m AHD, and the rehabilitated floor is finished at approximately 1.9 m AHD, leaving the site well above the maximum winter water table and comfortably in excess of the DWER minimums for a future pasture land use (DoW, 2014a). This adheres to the Developmental Approval (appendix 12) requirements which mandates 1.25m AHD (east side) and 1m AHD (west side), and well above the 0.5m requirement above the maximum seasonal level.

As set out in Section 3.4.2, this adopted maximum will be confirmed by direct on-site monitoring at the soak over the coming winter and the following summer — well before extraction advances anywhere near the groundwater level. Checking the levels against current on-site conditions before that depth is

worked, and holding a 1.4m clearance rather than the minimum, is protective of both the groundwater resource and the adjoining Lake Preston: should the soak readings show groundwater higher than the adopted figure, excavation simply stops higher again. The final landform is shown at Figure 4.

5.0 WATER MANAGEMENT MEASURES

Any extraction carries some risk to surrounding water resources, whether through storm water erosion of exposed ground or contamination. With Lake Preston — a Ramsar wetland — adjoining the lot, the chief water-quality risks are hydrocarbon pollution and sedimentation (weed risks are covered in the main report). The measures below mitigate these.

5.1 SURFACE WATER & BUFFERS

Lake Preston runs along the western boundary, outside the lot, and small Multiple Use wetlands sit in the northwest and northeast corners (Figure 1). No surface drainage lines occur within the site; drainage is internal and infiltrates to groundwater. DWER guidance recommends a 200 m buffer from sensitive water resources such as conservation wetlands like Lake Preston, and a 50 m buffer from Multiple Use wetlands (DoW, 2001); both are observed, as shown on Figure 1. The storm water measures below ensure no unmanaged surface runoff leaves the extraction area.

5.2 STORM WATER CONTAINMENT

An elevated ridge on the western side of the extraction area shields Lake Preston and its dependent vegetation from any runoff or sediment generated by high-frequency rainfall. Such runoff drains south to north toward the soak in the northeast of the property, though the high permeability of the ground materials means storm water issues are not expected.

Runoff within the extraction area for the 10-year, 2-hour ARI design storm has been calculated by the Rational Method using the 17.5 mm/hr intensity (BoM, 2026) and a disturbed-area runoff coefficient of 0.6 (ODOT, 2014), giving 756 m³ over the two-hour event for each 3.6 ha area (1,512 m³ across the whole footprint). To contain this, a detention pond of at least 760 m³ serves each of the two areas, sited along its northern boundary (Figure 2). The first pond is excavated to the base of the pit; the second is excavated, with cut-off drains diverting runoff into it, as the second area is opened, protecting the completed area for rehabilitation. Topsoil and overburden stockpiles placed along the southern boundary of each area act as bunds, keeping external runoff out of the pit. There will be no unmanaged surface runoff from the operation.

5.3 GROUNDWATER PROTECTION

No dewatering is undertaken and no groundwater is permanently exposed, since the final surface sits 500 mm above the maximum winter groundwater table, consistent with DWER guidance (DoW, 2014a). Excavation stops 300 mm above the maximum groundwater level, at 0.491 m AHD (DoW, 2014a).

Water needs are minor and limited to dust suppression, drawn from the on-site soak under the groundwater abstraction license; this draw is not expected to materially affect local groundwater levels. Given the small scale of the operation no groundwater contamination is anticipated. No fuel or lubricant

is stored on site; refueling uses a mobile vehicle fitted with a snap-on/snap-off, fast-fill, auto-shut-off system, with plant fueled each morning so vehicles sit near-empty overnight. Major servicing — the main spill risk — is carried out at the operator's Finn Road workshop rather than on site. A Hydrocarbon Spill Management Plan is provided as Addendum 2. During rehabilitation, fertilizer is applied in consultation with the Department of Primary Industries and Regional Development at appropriate rates; correct application and the clayey subsurface limit nutrient leaching. Herbicide is used only as needed, with preference for soil-binding, low-leaching products, and use declines as vegetation establishes.

5.4 MONITORING & MAINTENANCE

Through extraction and early rehabilitation the pit is inspected after each significant rainfall event for erosion, with any repairs made immediately. Following closure, rehabilitated areas are monitored annually for landform stability, success of the sown pasture, and weed emergence, continuing until the completion criteria are met. Maintenance, where required, may include repairing erosion, re-seeding failed areas, and weed control.

5.5 ACID SULPHATE SOILS

Through extraction and early rehabilitation the pit is inspected after each significant rainfall event for erosion, with any repairs made immediately. Following closure, rehabilitated areas are monitored annually for landform stability, success of the sown pasture, and weed emergence, continuing until the completion criteria are met. Maintenance, where required, may include repairing erosion, re-seeding failed areas, and weed control.

Potential acid sulphate soils (ASS) on the Swan Coastal Plain are mapped by the former Department of Environment and Conservation (now DWER) (DEC, 2006), accessed via Landgate (Landgate, 2026), in two risk classes — Class 1 (moderate to high risk within 3 m of the surface) and Class 2 (low to moderate risk within 3 m). The mapping shows a small Class 1 area (about 0.3 ha) at the center of the northern edge of the extraction area; the southwest corner carries no known ASS risk; and the remainder (roughly two-thirds, along the north and west) is Class 2 (Figure 3). These soils are associated with the wetlands to the west (Lake Preston) and north.

Because extraction stays above the water table and no dewatering occurs, no ASS will be exposed to oxygen. Before the first detention pond (which falls within the Class 1 area) is excavated, a preliminary dig will check whether ASS material is present; if it is, the pond will be relocated east or west to the most suitable position and surface bunding used to direct storm water into it.

6.0 REFERENCES

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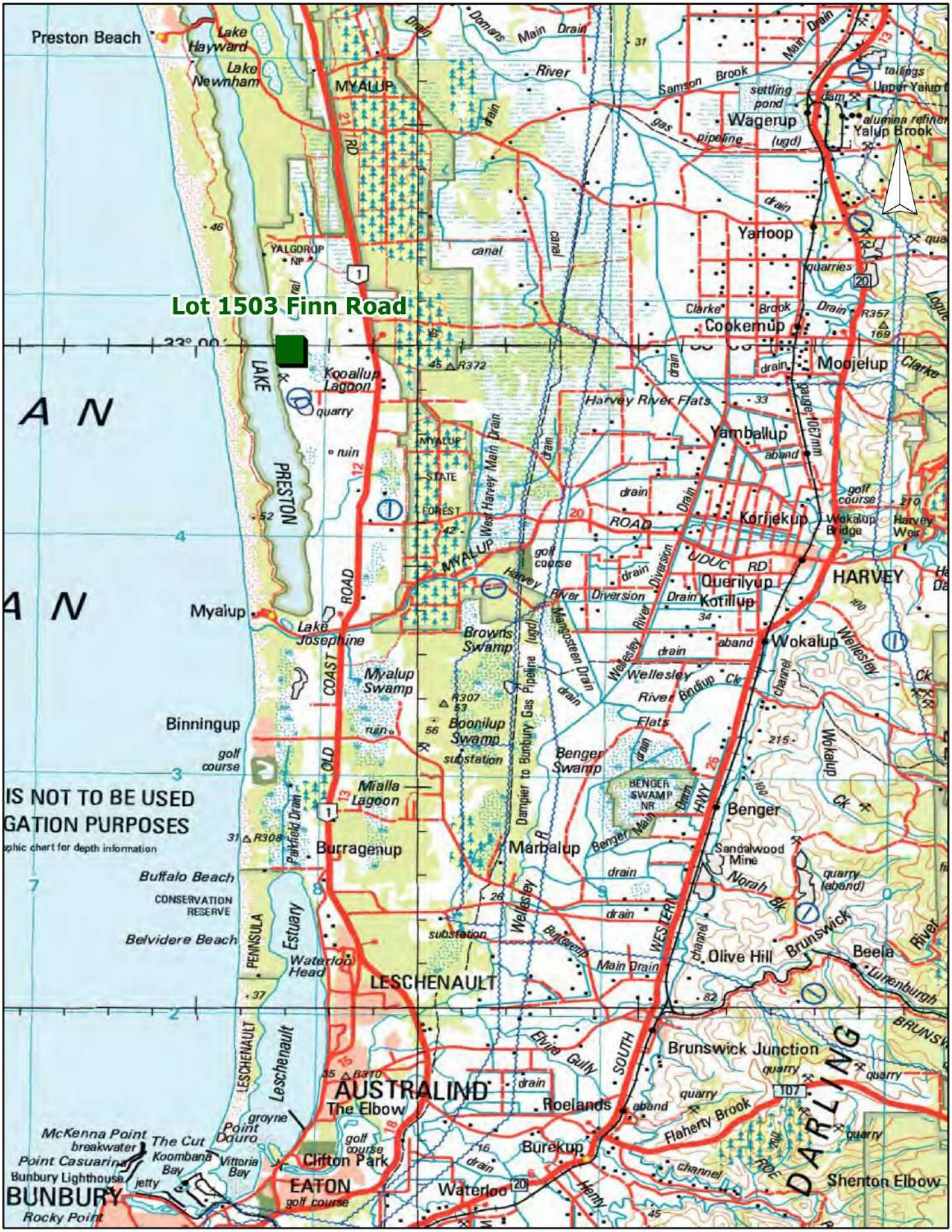
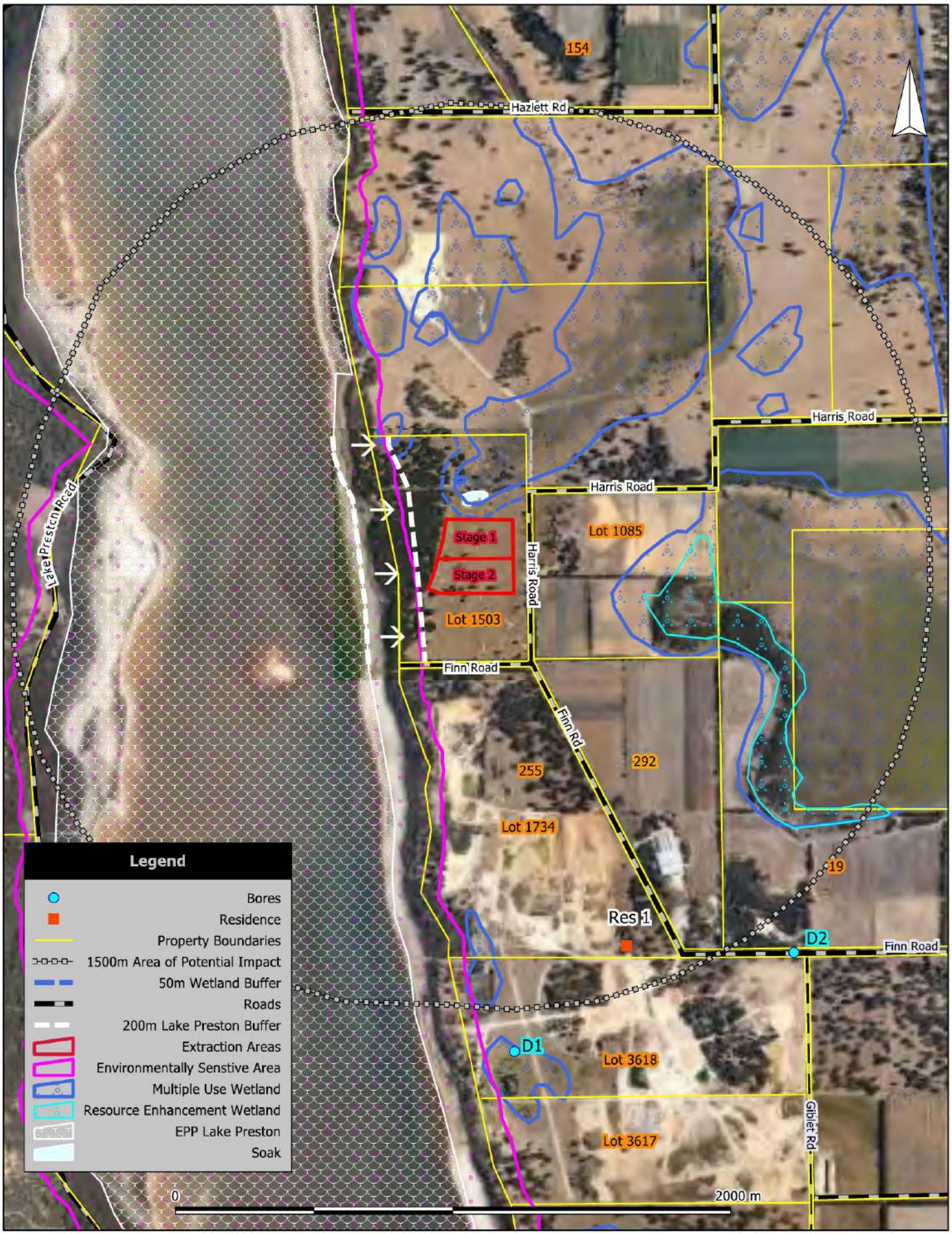
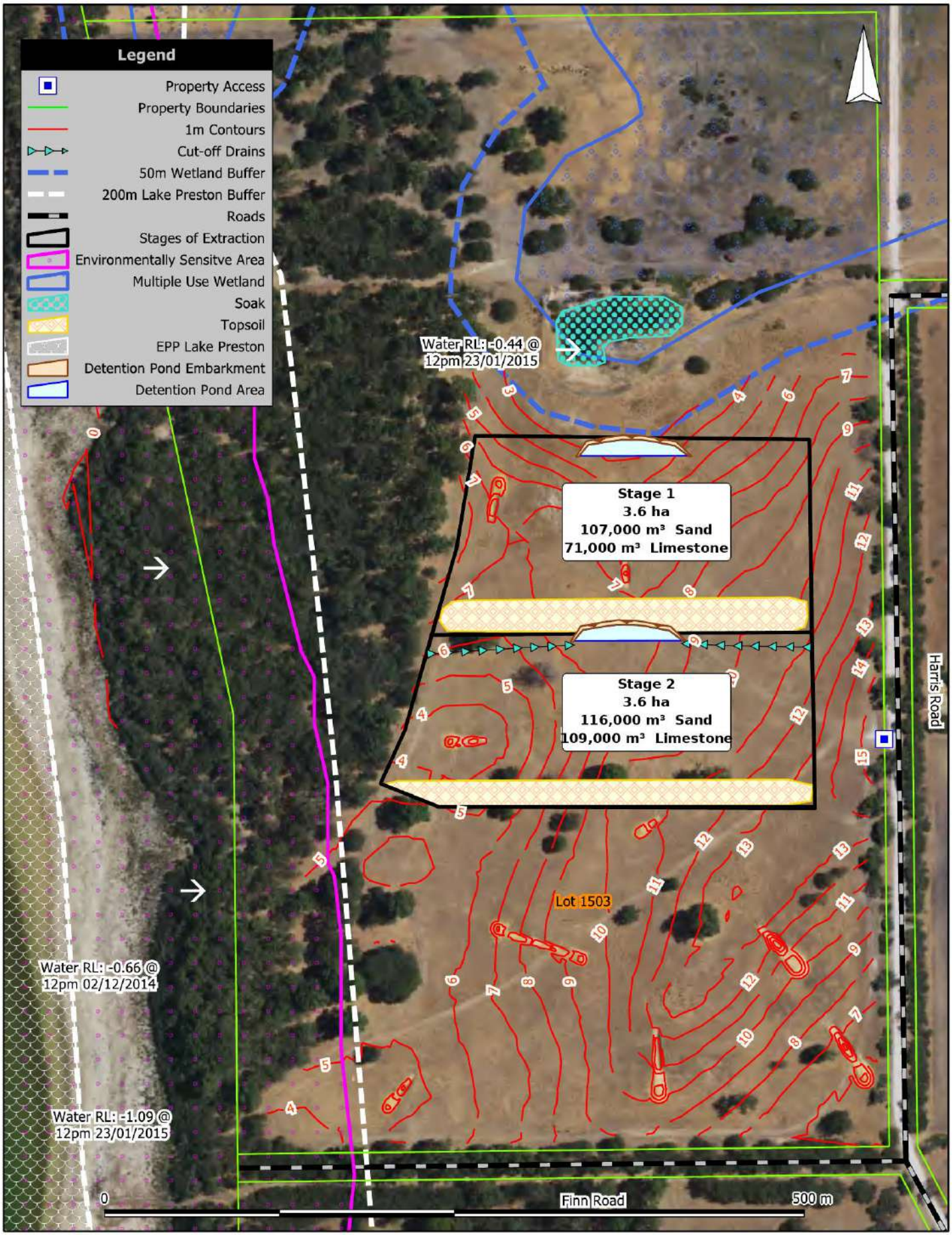


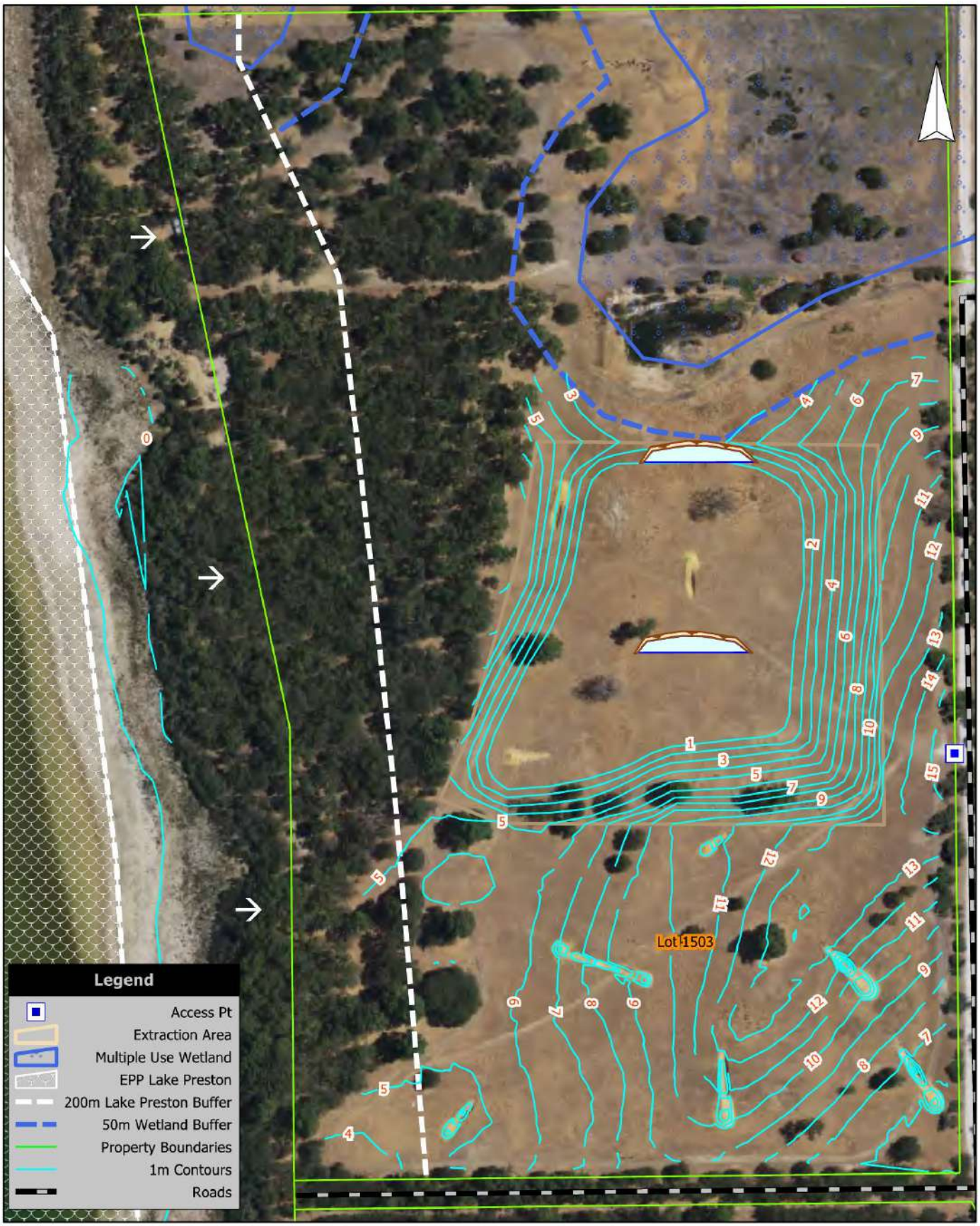
Lundstrom Environmental Consultants Pty Ltd 21 Sellen Ct Leeming WA 6149 Mobile: 0417934863 mikelund1@bigpond.com	Scale: 1:5600 Original Size: A4 Source: NATMAP Digital Maps 2008 Datum: GDA94	**Omaha Nominees Pty Ltd** **Lot 1503 Finn Road MYALUP**	**Locality** **Figure 1**



Lundstrom Environmental Consultants Pty Ltd 21 Sellen Ct Leeming WA 6149 Mobile: 0417934863 mikelund1@bigpond.com	Scale: 1:17000 Original Size: A4 Air Photo Date: Landcorp February 2014 Datum: Australian Geocentric 1994 (GDA94)	**Omaha Nominees Pty Ltd** **1503 Harris Road MYALUP**	**Site and Surrounds** **Figure 2**



Lundstrom Environmental Consultants Pty Ltd **21 Sellen Ct Leeming WA 6149** **Mobile: 0417934863** **mikelund1@bigpond.com**	Scale: 1:3500 Original Size: A4 Air Photo Date: Landcorp February 2014 Datum: Australian Geocentric 1994 (GDA94	**Omaha Nominees Pty Ltd** **1503 Harris Road MYALUP**	**Extraction Area** **Figure 3**



Lundstrom Environmental Consultants Pty Ltd **21 Sellen Ct Leeming WA 6149** **Mobile: 0417934863** **mikelund1@bigpond.com**	Scale: 1:3500 Original Size: A4 Air Photo Date: Landcorp February 2014 Datum: Australian Geocentric 1994 (GDA94	**Omaha Nominees Pty Ltd** **1503 Harris Road MYALUP**	**Final Land Surface** **Figure 4**

ADDENDUM 1

Hydrograph Monitoring of Bores D1,D2,LPNSWIM

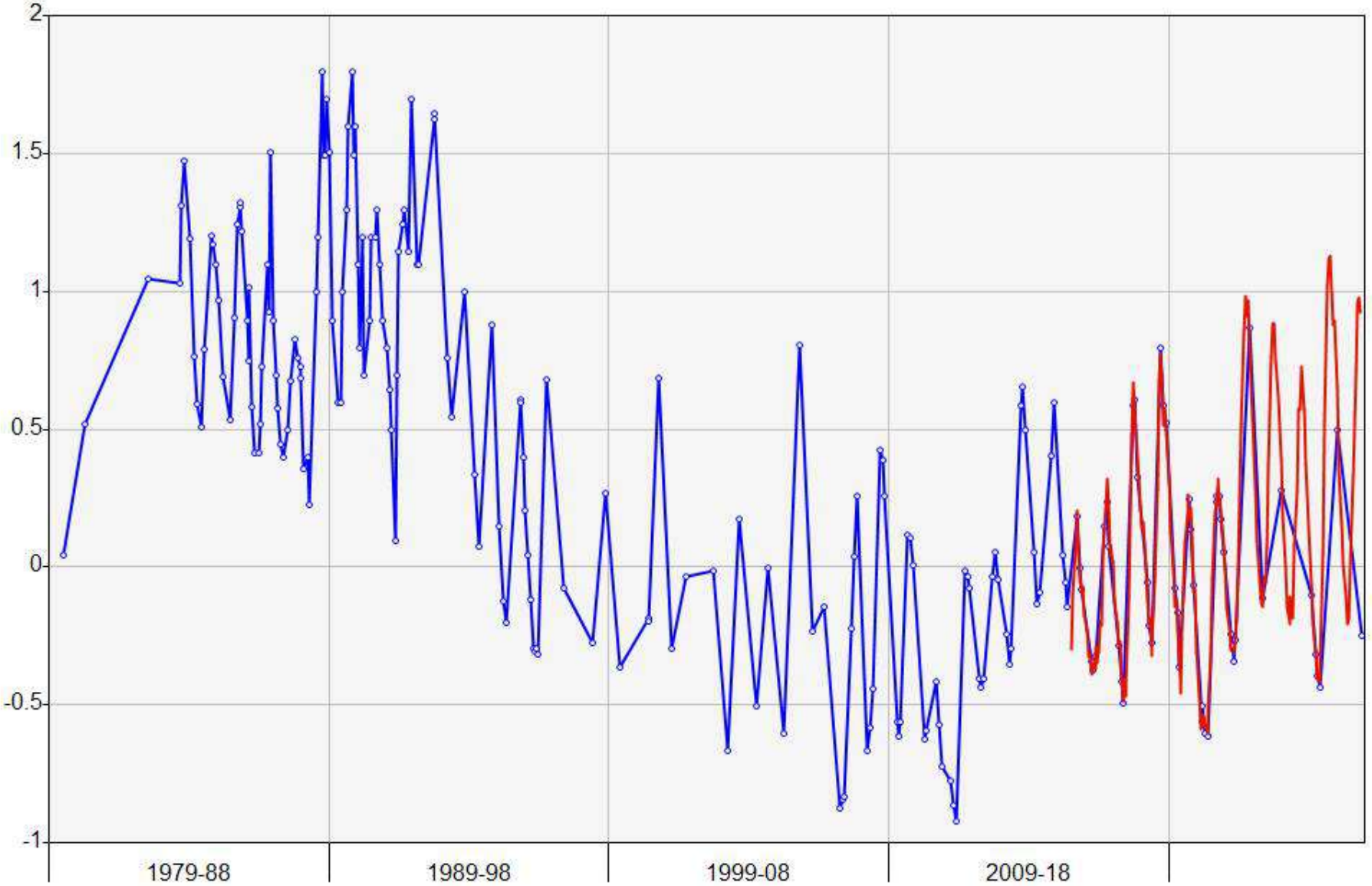
Department of Water and Environmental Regulation

HYPLOT V135 Output 06/12/2025

Period 47 Year 01/01/1979 to 01/01/2026 1979-2025

61319145 Lake Clifton D2 Water Level (mAHD) GW

61319145 Lake Clifton D2 Water Level (mAHD) A



Department of Water and Environmental Regulation

HYPLOT V135 Output 11/12/2025

Period 6 Year 01/01/2020 to 01/01/2026 2020-25

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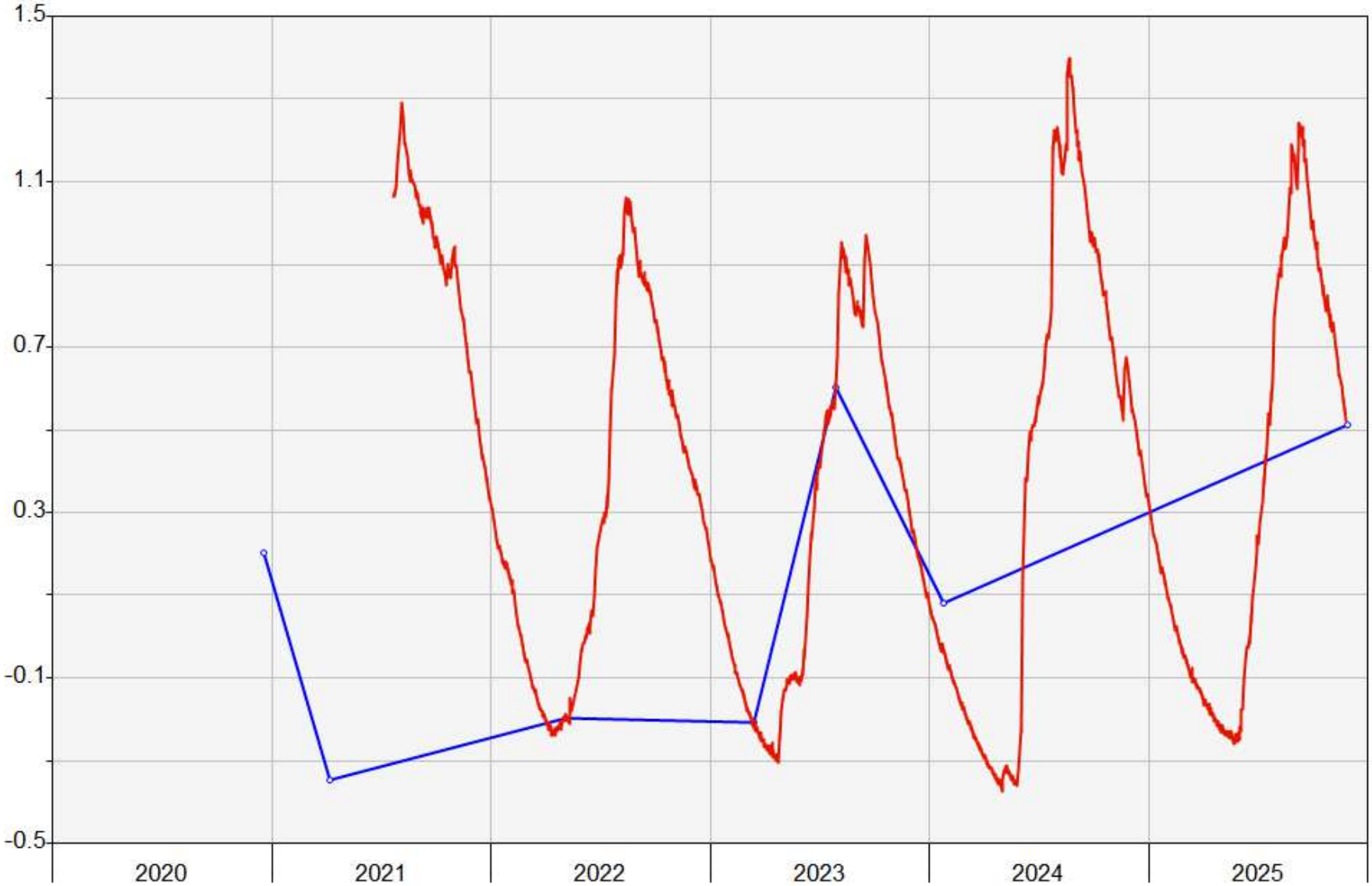
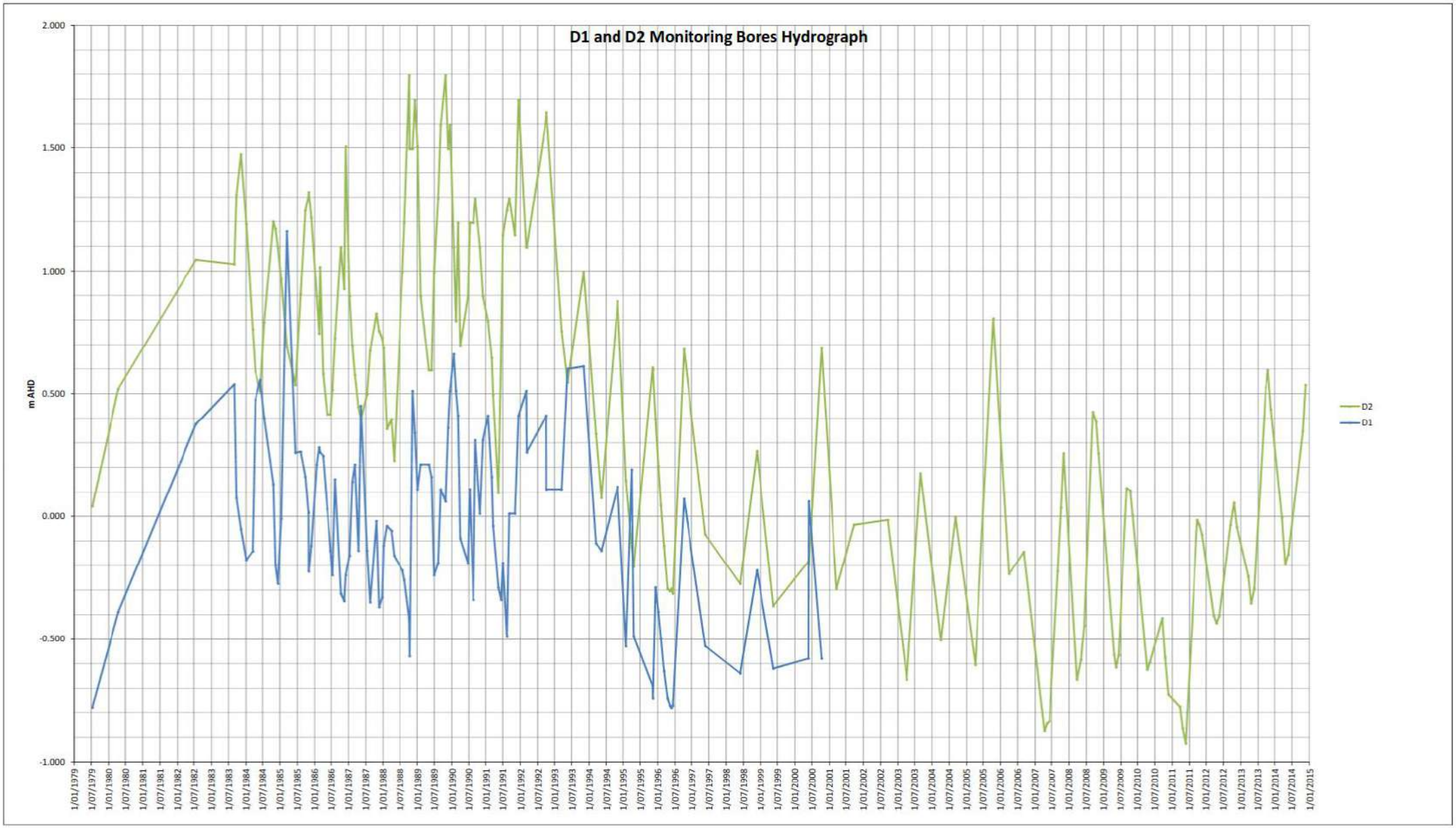
61370121 LPNSWIM 04-20 Water Level (mAHD) A




D1 and D2 Monitoring Bores Hydrograph
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ADDENDUM 2

Hydrocarbon Spill Management

HYDROCARBON SPILL MANAGEMENT PLAN

Purpose

This Hydrocarbon Spill Management Plan isto limit the impact of any hydrocarbon spill that may occur on the extraction site and to protect soil, groundwater and the adjoining Lake Preston.

Preventative measures

The following measures are in place to avoid spills occurring in the first place:

- No fuel is stored on the site. Plant and equipment are refueled as required by a mobile fuel truck, with refueling carried out in the morning so that machines sit close to empty overnight.
- Refueling trucks are fitted with automatic snap-off nozzles, which prevent overfilling and the spillage that can result from it.
- Major servicing — the activity most likely to produce a fuel or oil spill — is carried out away from the site, at the workshop on Lot 3618 Finn Road.
- Operators and drivers are briefed on hydrocarbon pollution prevention as part of their site induction.

Response in the event of a spill

Should a spill nonetheless occur, the following steps are taken, in order:

- Stop the source of the spill straight away, where it is safe to do so.
- Contain the spill and keep it away from any drains and water bodies.
- Recover the spill by excavating the contaminated soil and carting it to a licensed waste disposal facility, then back filling the excavation with clean fill.
- Where practical, keep a photographic record of the spill and the clean-up.
- Report the incident to the Quarry Manager.